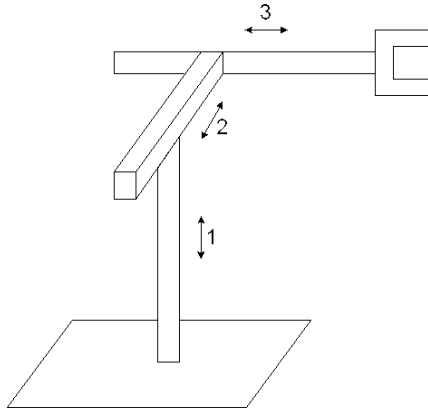


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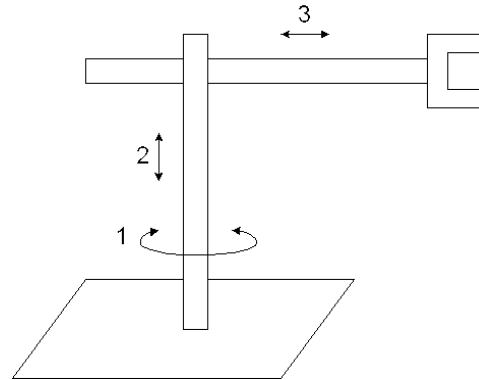
# Kinematics II

# Review

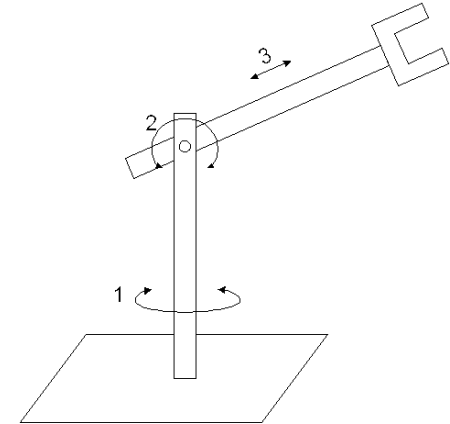
- Manipulators:



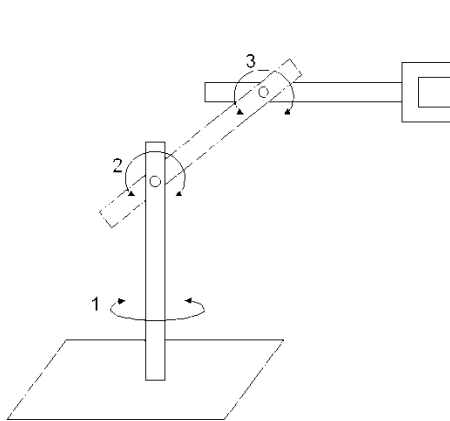
Cartesian: PPP



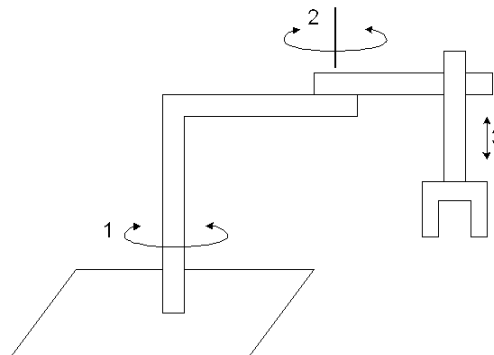
Cylindrical: RPP



Spherical: RRP

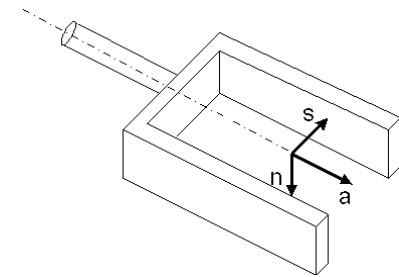


Articulated: RRR



SCARA: RRP

(Selective Compliance Assembly Robot Arm)



Hand coordinate:

**n**: normal vector; **s**: sliding vector;

**a**: approach vector, normal to the tool mounting plate

# Basic Rotation Matrices

- Rotation about x-axis with  $\theta$

$$Rot(x, \theta) = \begin{bmatrix} 1 & 0 & 0 \\ 0 & C\theta & -S\theta \\ 0 & S\theta & C\theta \end{bmatrix}$$

- Rotation about y-axis with  $\theta$

$$Rot(y, \theta) = \begin{bmatrix} C\theta & 0 & S\theta \\ 0 & 1 & 0 \\ -S\theta & 0 & C\theta \end{bmatrix}$$

- Rotation about z-axis with  $\theta$

$$P_{xyz} = RP_{uvw} \quad Rot(z, \theta) = \begin{bmatrix} C\theta & -S\theta & 0 \\ S\theta & C\theta & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

# Review

---

- Composite Homogeneous Transformation Matrix
- Rules:
  - Transformation (rotation/translation) w.r.t.  $(X, Y, Z)$  (OLD FRAME), using **pre-multiplication**
  - Transformation (rotation/translation) w.r.t.  $(U, V, W)$  (NEW FRAME), using **post-multiplication**

# Review

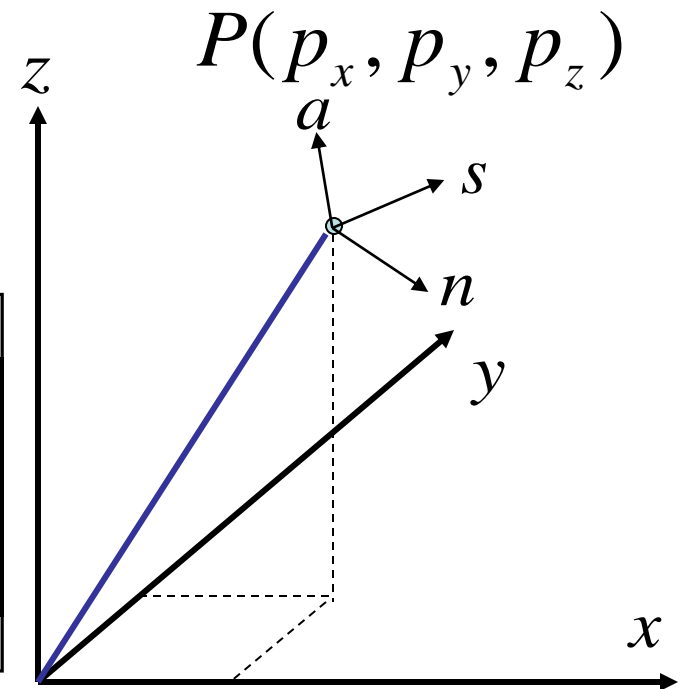
- Homogeneous Representation

- A point in  $R^3$  space

$$P = \begin{bmatrix} p_x \\ p_y \\ p_z \\ 1 \end{bmatrix} \leftarrow \text{Homogeneous coordinate of } P \text{ w.r.t. OXYZ}$$

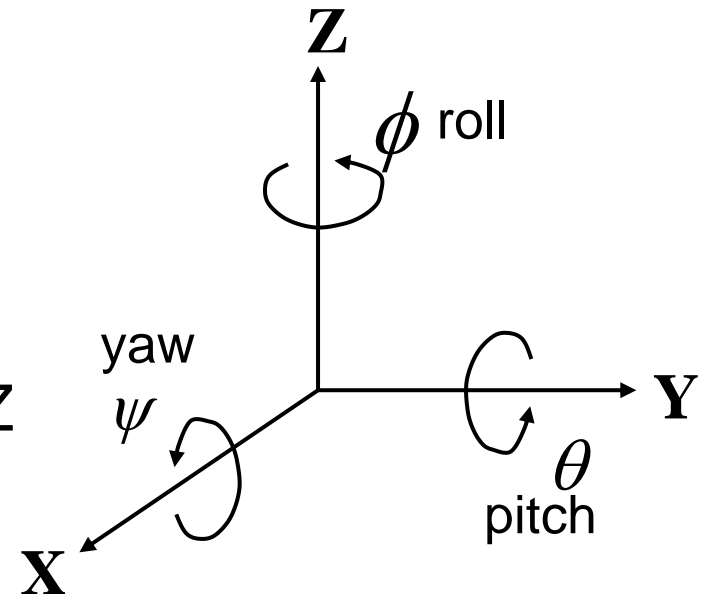
- A frame in  $R^3$  space

$$F = \begin{bmatrix} n & s & a & P \\ 0 & 0 & 0 & 1 \end{bmatrix} = \begin{bmatrix} n_x & s_x & a_x & p_x \\ n_y & s_y & a_y & p_y \\ n_z & s_z & a_z & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



# Review

- Orientation Representation (Euler Angles)
  - Description of Yaw, Pitch, Roll
    - A rotation of  $\psi$  about the OX axis ( $R_{x,\psi}$ ) -- yaw
    - A rotation of  $\theta$  about the OY axis ( $R_{y,\theta}$ ) -- pitch
    - A rotation of  $\phi$  about the OZ axis ( $R_{z,\phi}$ ) -- roll

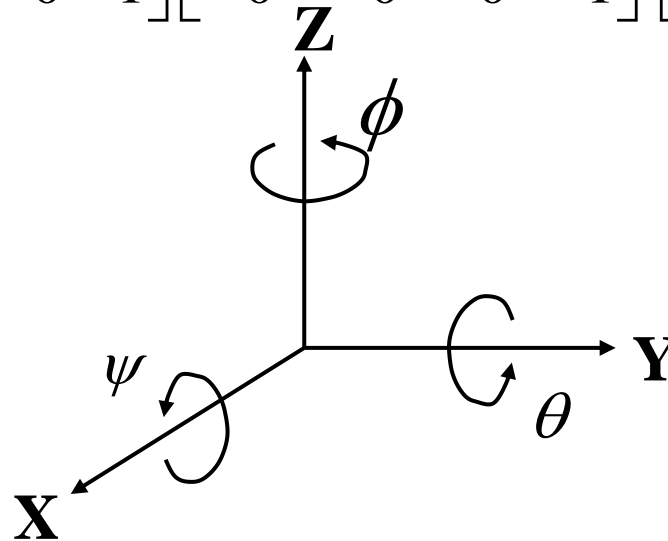


# Quiz 1

- How to get the resultant rotation matrix for YPR?

$$T = R_{z,\phi} R_{y,\theta} R_{x,\psi}$$

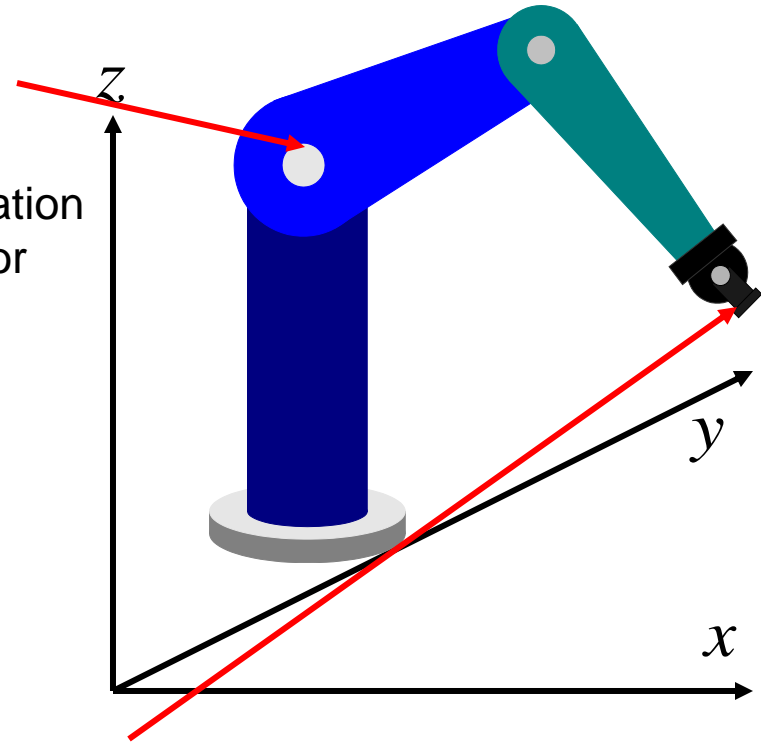
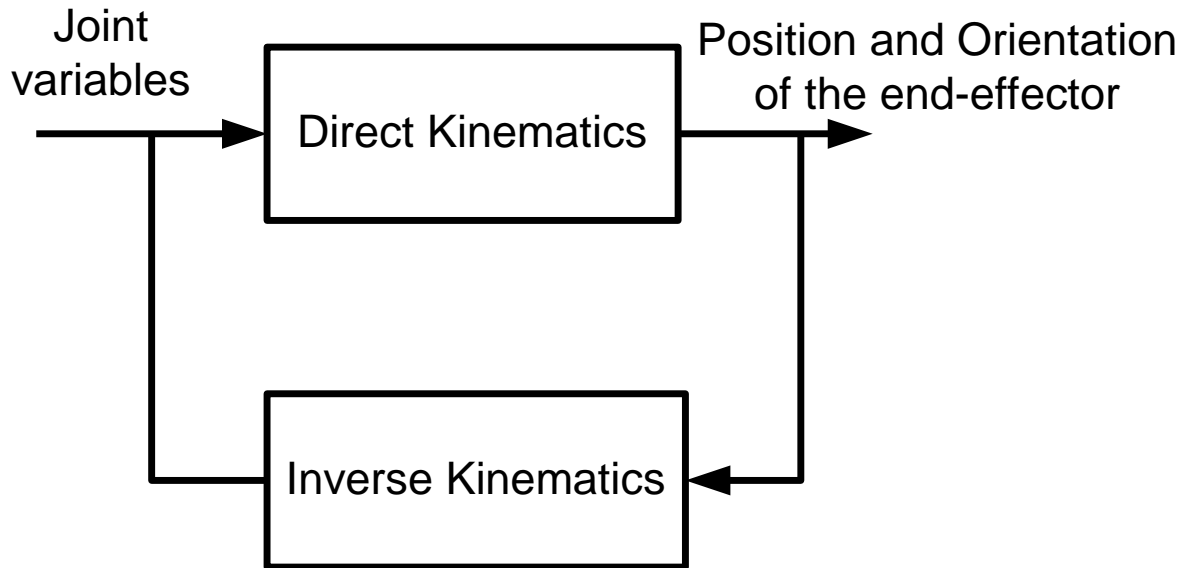
$$= \begin{bmatrix} C\phi & -S\phi & 0 & 0 \\ S\phi & C\phi & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} C\theta & 0 & S\theta & 0 \\ 0 & 1 & 0 & 0 \\ -S\theta & 0 & C\theta & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & C\psi & -S\psi & 0 \\ 0 & S\psi & C\psi & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$



# Kinematics Model

- Forward (direct) Kinematics

$$q = (q_1, q_2, \dots, q_n)$$



$$Y = (x, y, z, \phi, \theta, \psi)$$

- Inverse Kinematics

*Robotics*

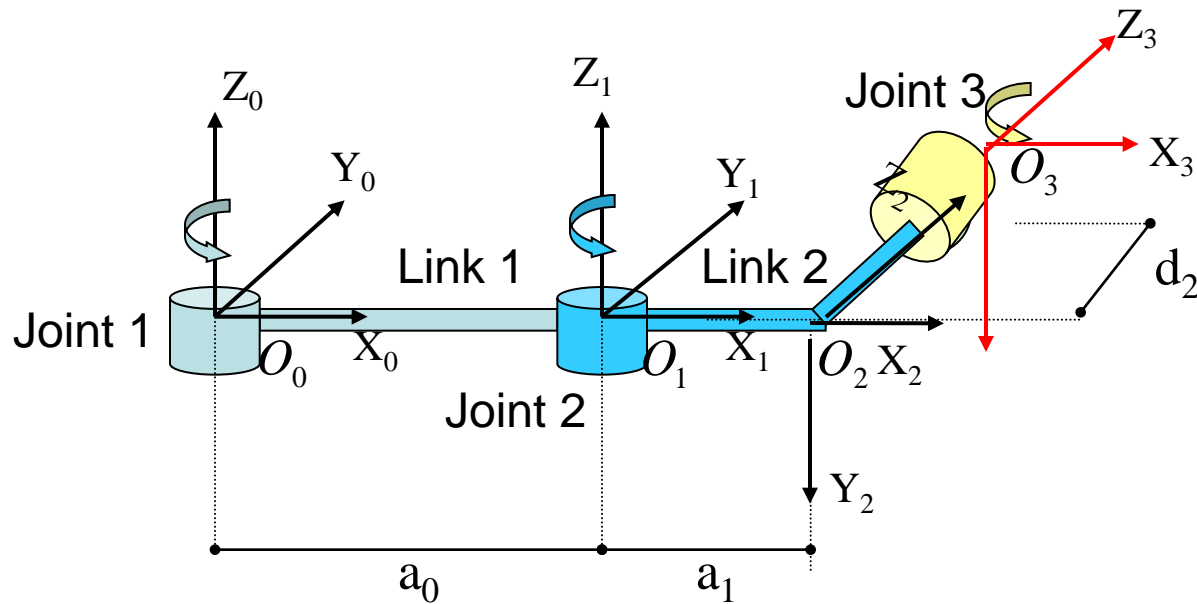


# Denavit-Hartenberg Convention

- Number the joints from 1 to n starting with the base and ending with the end-effector.
- *Establish the base coordinate system.* Establish a right-handed orthonormal coordinate system  $(X_0, Y_0, Z_0)$  at the supporting base with  $Z_0$  axis lying along the axis of motion of joint 1.
- *Establish joint axis.* Align the  $Z_i$  with the axis of motion (rotary or sliding) of joint  $i+1$ .
- *Establish the origin of the  $i$ th coordinate system.* Locate the origin of the  $i$ th coordinate at the intersection of the  $Z_i$  &  $Z_{i-1}$  or at the intersection of common normal between the  $Z_i$  &  $Z_{i-1}$  axes and the  $Z_i$  axis.
- *Establish  $X_i$  axis.* Establish  $X_i = \pm(Z_{i-1} \times Z_i) / \|Z_{i-1} \times Z_i\|$  or along the common normal between the  $Z_{i-1}$  &  $Z_i$  axes when they are parallel.
- *Establish  $Y_i$  axis.* Assign  $Y_i = +(Z_i \times X_i) / \|Z_i \times X_i\|$  to complete the right-handed coordinate system.
- Find the link and joint parameters

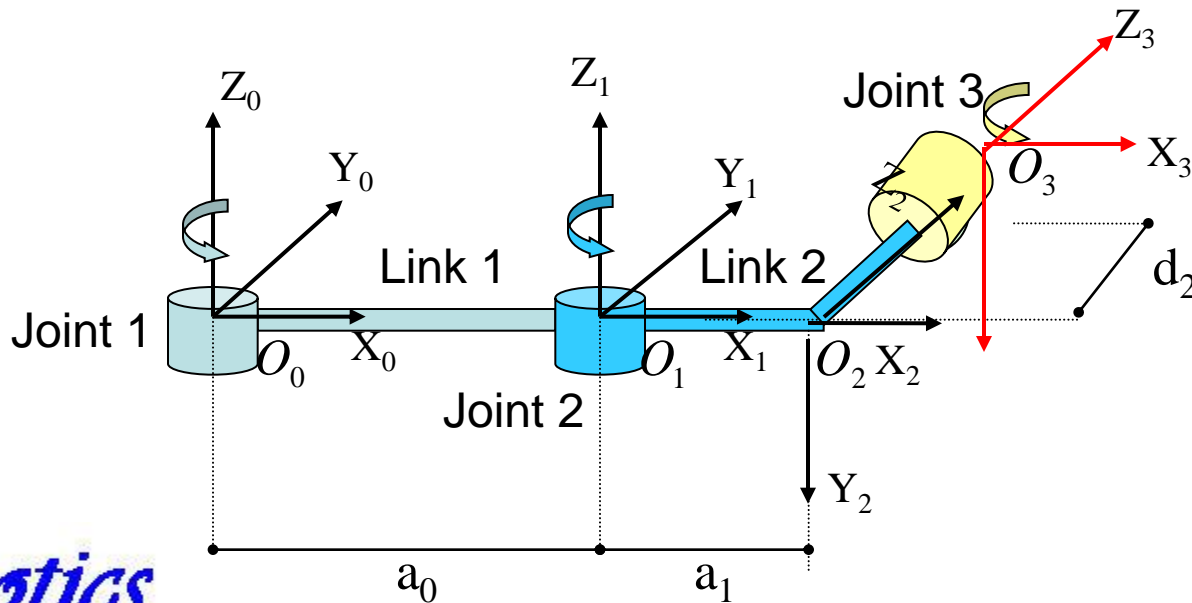
# Example I

- 3 Revolute Joints



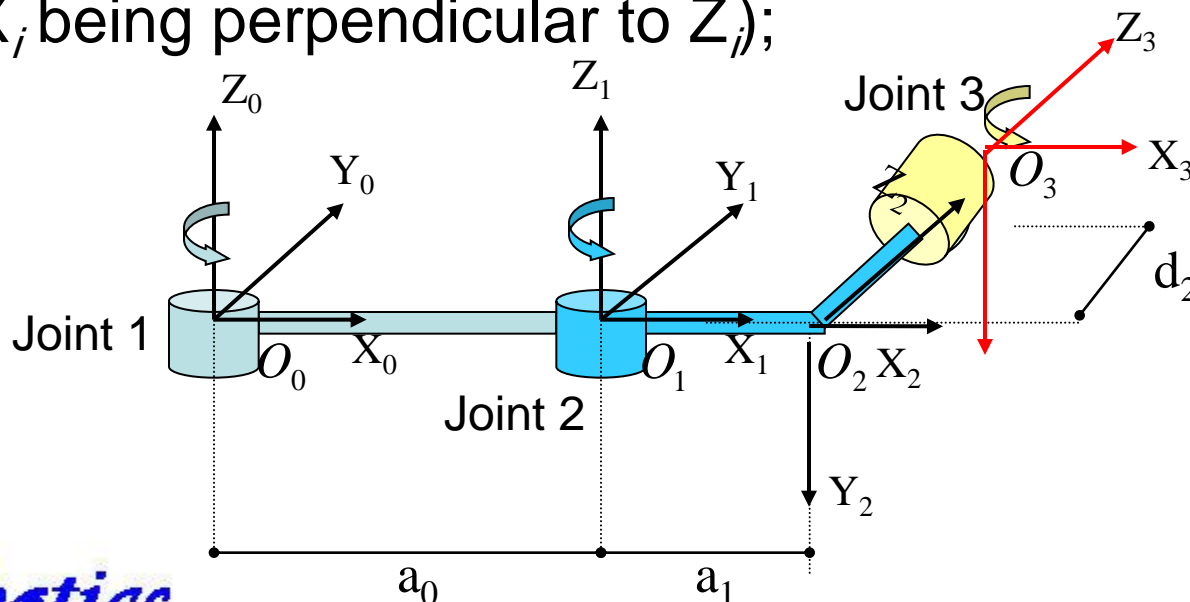
# Link Coordinate Frames

- *Assign Link Coordinate Frames:*
  - To describe the geometry of robot motion, we assign a Cartesian coordinate frame  $(O_i, X_i, Y_i, Z_i)$  to each link, as follows:
    - establish a right-handed orthonormal coordinate frame  $O_0$  at the supporting base with  $Z_0$  lying along joint 1 motion axis.
    - the  $Z_i$  axis is directed along the axis of motion of joint  $(i+1)$ , that is, link  $(i+1)$  rotates about or translates along  $Z_i$ ;



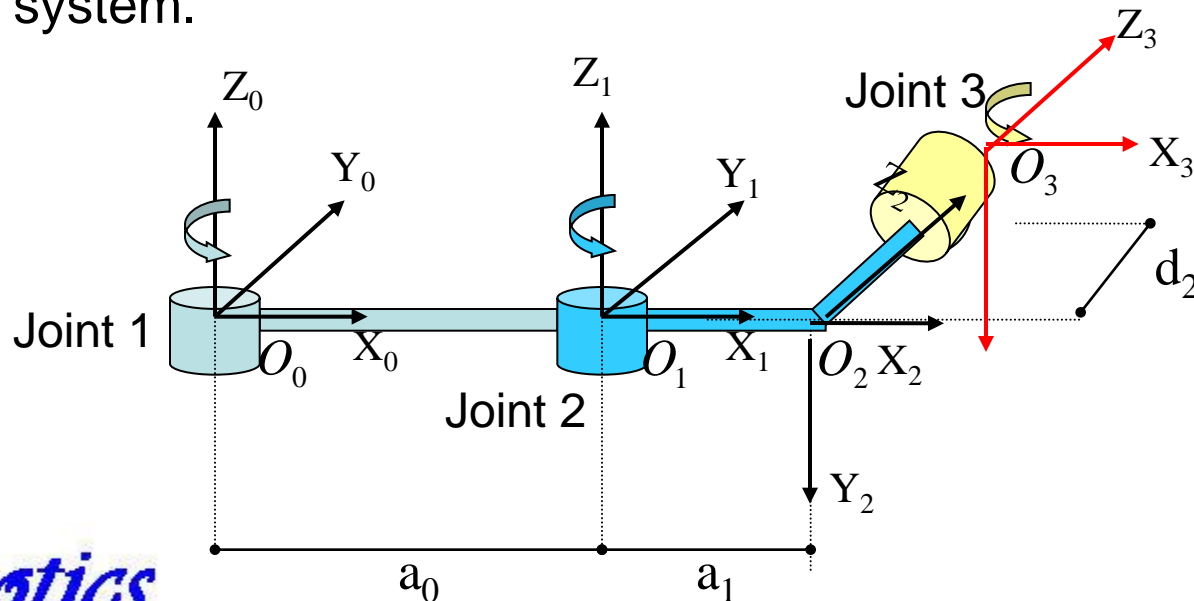
# Link Coordinate Frames

- Locate the origin of the  $i$ th coordinate at the intersection of the  $Z_i$  &  $Z_{i-1}$  or at the intersection of common normal between the  $Z_i$  &  $Z_{i-1}$  axes and the  $Z_i$  axis.
- the  $X_i$  axis lies along the common normal from the  $Z_{i-1}$  axis to the  $Z_i$  axis  $X_i = \pm(Z_{i-1} \times Z_i) / \|Z_{i-1} \times Z_i\|$ , (if  $Z_{i-1}$  is parallel to  $Z_i$ , then  $X_i$  is specified arbitrarily, subject only to  $X_i$  being perpendicular to  $Z_i$ );



# Link Coordinate Frames

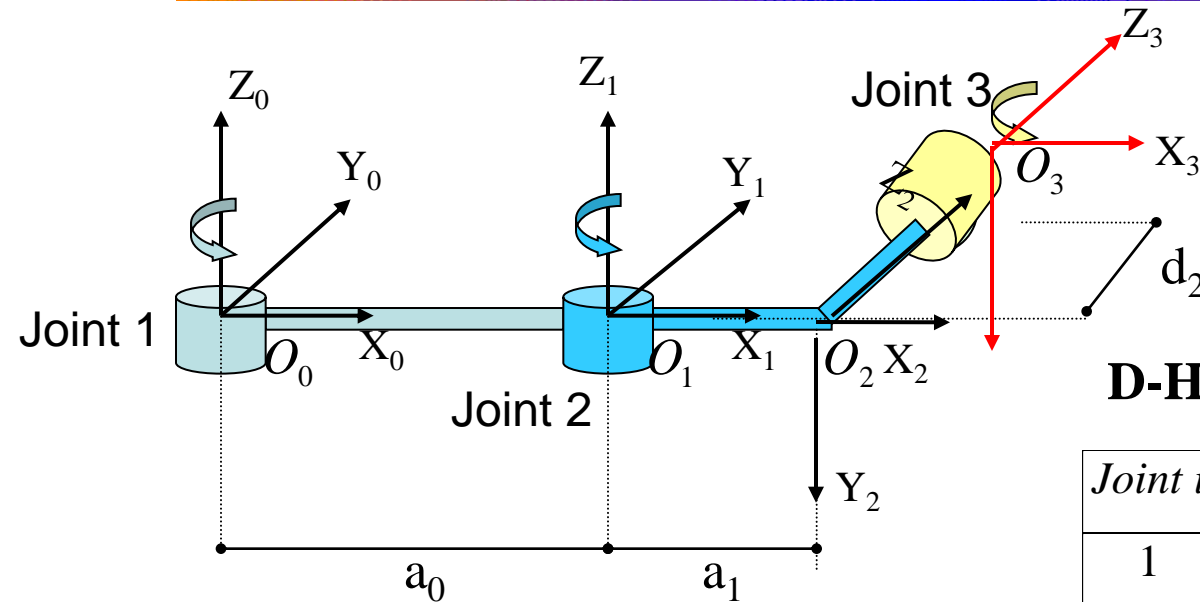
- Assign  $Y_i = +(Z_i \times X_i) / \|Z_i \times X_i\|$  to complete the right-handed coordinate system.
- The hand coordinate frame is specified by the geometry of the end-effector. Normally, establish  $Z_n$  along the direction of  $Z_{n-1}$  axis and pointing away from the robot; establish  $X_n$  such that it is normal to both  $Z_{n-1}$  and  $Z_n$  axes. Assign  $Y_n$  to complete the right-handed coordinate system.



# Link and Joint Parameters

- **Joint angle**  $\theta_i$ : the angle of rotation from the  $X_{j-1}$  axis to the  $X_j$  axis about the  $Z_{j-1}$  axis. It is the joint variable if joint  $i$  is rotary.
- **Joint distance**  $d_i$ : the distance from the origin of the  $(i-1)$  coordinate system to the intersection of the  $Z_{i-1}$  axis and the  $X_i$  axis along the  $Z_{i-1}$  axis. It is the joint variable if joint  $i$  is prismatic.
- **Link length**  $a_i$ : the distance from the intersection of the  $Z_{i-1}$  axis and the  $X_i$  axis to the origin of the  $i$ th coordinate system along the  $X_i$  axis.
- **Link twist angle**  $\alpha_i$ : the angle of rotation from the  $Z_{i-1}$  axis to the  $Z_i$  axis about the  $X_i$  axis.

# Example I



**D-H Link Parameter Table**

Joint $i$	$\alpha_i$	$a_i$	$d_i$	$\theta_i$
1	0	$a_0$	0	$\theta_0$
2	-90	$a_1$	0	$\theta_1$
3	0	0	$d_2$	$\theta_2$

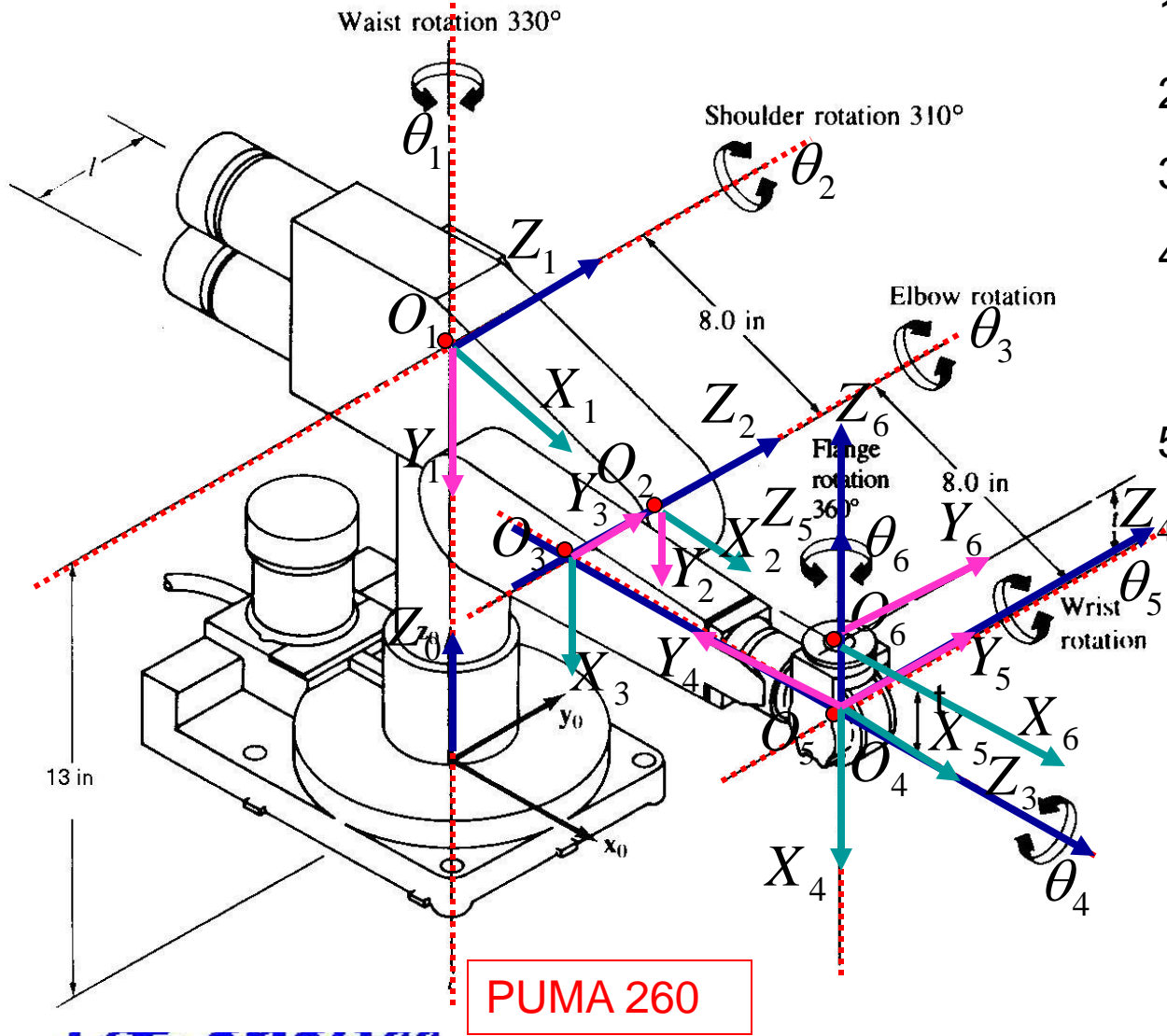
$\alpha_i$  : rotation angle from  $Z_{i-1}$  to  $Z_i$  about  $X_i$

$a_i$  : distance from intersection of  $Z_{i-1}$  &  $X_i$  to origin of  $i$  coordinate along  $X_i$

$d_i$  : distance from origin of  $(i-1)$  coordinate to intersection of  $Z_{i-1}$  &  $X_i$  along  $Z_{i-1}$

$\theta_i$  : rotation angle from  $X_{i-1}$  to  $X_i$  about  $Z_{i-1}$

# Example II: PUMA 260



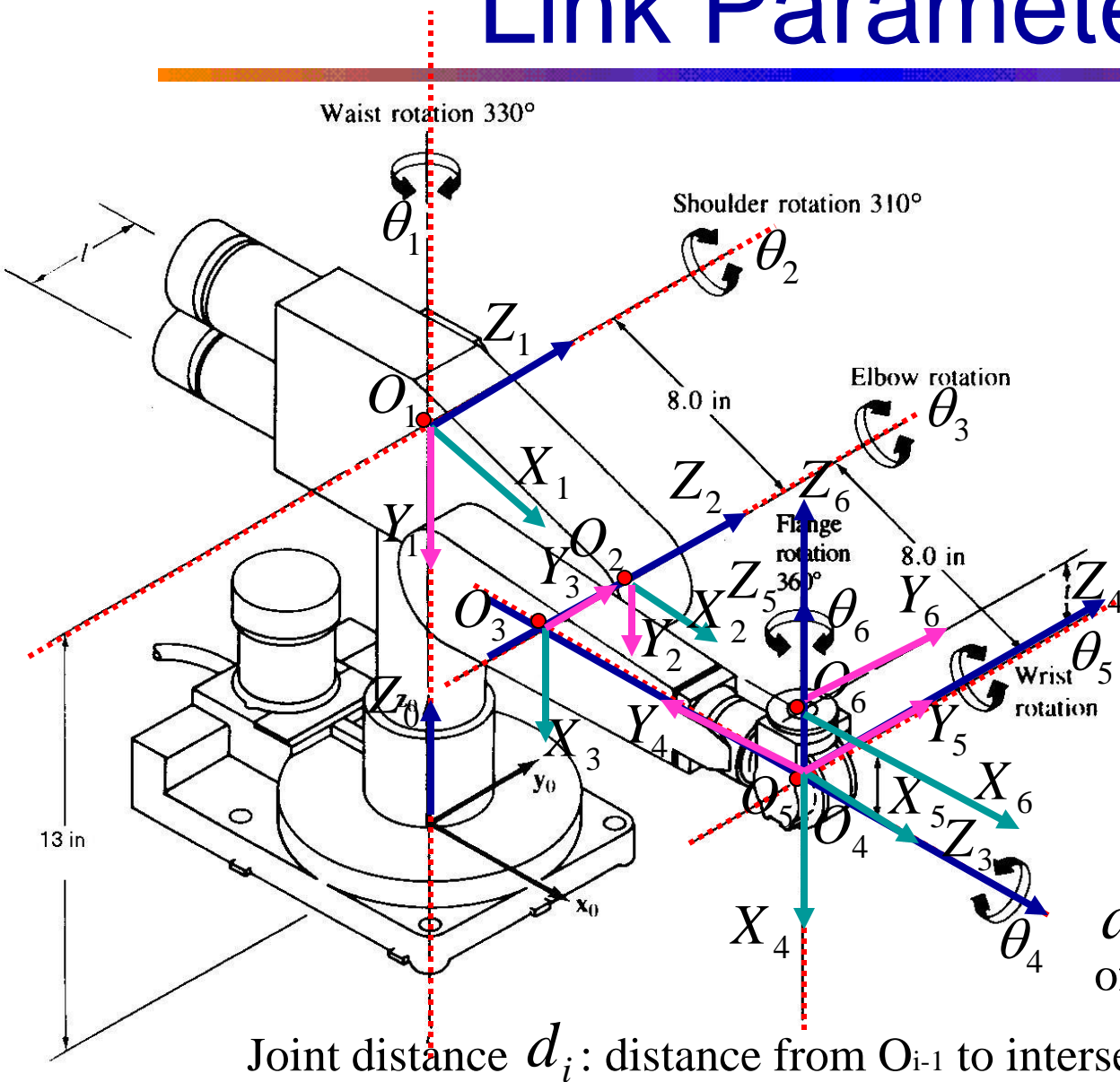
1. Number the joints
2. Establish base frame
3. Establish joint axis  $Z_i$
4. Locate origin, (intersect. of  $Z_i$  &  $Z_{i-1}$ ) OR (intersect of common normal &  $Z_i$ )
5. Establish  $X_i, Y_i$

$$X_i = \pm(Z_{i-1} \times Z_i) / \|Z_{i-1} \times Z_i\|$$

$$Y_i = +(Z_i \times X_i) / \|Z_i \times X_i\|$$



# Link Parameters



J	$\theta_i$	$\alpha_i$	$a_i$	$d_i$
1	$\theta_1$	-90	0	13
2	$\theta_2$	0	8	0
3	$\theta_3$	90	0	-l
4	$\theta_4$	-90	0	8
5	$\theta_5$	90	0	0
6	$\theta_6$	0	0	t

$\theta_i$ : angle from  $X_{i-1}$  to  $X_i$  about  $Z_{i-1}$

$\alpha_i$ : angle from  $Z_{i-1}$  to  $Z_i$  about  $X_i$

$a_i$ : distance from intersection of  $Z_{i-1}$  &  $X_i$  to  $O_i$  along  $X_i$

# Transformation between $i-1$ and $i$

- Four successive elementary transformations are required to relate the  $i$ -th coordinate frame to the  $(i-1)$ -th coordinate frame:
  - Rotate about the  $Z_{i-1}$  axis an angle of  $\theta_i$  to align the  $X_{i-1}$  axis with the  $X_i$  axis.
  - Translate along the  $Z_{i-1}$  axis a distance of  $d_i$ , to bring  $X_{i-1}$  and  $X_i$  axes into coincidence.
  - Translate along the  $X_i$  axis a distance of  $a_i$  to bring the two origins  $O_{i-1}$  and  $O_i$  as well as the  $X$  axis into coincidence.
  - Rotate about the  $X_i$  axis an angle of  $\alpha_i$  ( in the right-handed sense), to bring the two coordinates into coincidence.

# Transformation between $i-1$ and $i$

- D-H transformation matrix for adjacent coordinate frames,  $i$  and  $i-1$ .
  - The position and orientation of the  $i$ -th frame coordinate can be expressed in the  $(i-1)$ th frame by the following homogeneous transformation matrix:

Source coordinate

$$T_{i-1}^i = T(z_{i-1}, d_i)R(z_{i-1}, \theta_i)T(x_i, a_i)R(x_i, \alpha_i)$$

Reference Coordinate

$$\begin{bmatrix} C\theta_i & -C\alpha_i S\theta_i & S\alpha_i S\theta_i & a_i C\theta_i \\ S\theta_i & C\alpha_i C\theta_i & -S\alpha_i C\theta_i & a_i S\theta_i \\ 0 & S\alpha_i & C\alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Kinematic Equations

- Forward Kinematics  $q = (q_1, q_2, \dots, q_n)$ 
  - Given joint variables
  - End-effector position & orientation  $Y = (x, y, z, \phi, \theta, \psi)$
- Homogeneous matrix  $T_0^n$ 
  - specifies the location of the  $i$ th coordinate frame w.r.t. the base coordinate system
  - chain product of successive coordinate transformation matrices of  $T_{i-1}^i$

$$T_0^n = T_0^1 T_1^2 \dots T_{n-1}^n$$

$$= \begin{bmatrix} R_0^n & P_0^n \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} n & s & a & P_0^n \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Orientation matrix

Position vector

# Kinematics Equations

- Other representations
  - reference from, tool frame

$$T_{ref}^{tool} = B_{ref}^0 T_0^n H_n^{tool}$$

- Yaw-Pitch-Roll representation for orientation

$$T = R_{z,\phi} R_{y,\theta} R_{x,\psi}$$
$$= \begin{bmatrix} C\phi & -S\phi & 0 & 0 \\ S\phi & C\phi & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} C\theta & 0 & S\theta & 0 \\ 0 & 1 & 0 & 0 \\ -S\theta & 0 & C\theta & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & C\psi & -S\psi & 0 \\ 0 & S\psi & C\psi & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Representing forward kinematics

- Forward kinematics
- Transformation Matrix

$$\begin{bmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \\ \theta_4 \\ \theta_5 \\ \theta_6 \end{bmatrix} \Rightarrow \begin{bmatrix} p_x \\ p_y \\ p_z \\ \phi \\ \theta \\ \varphi \end{bmatrix}$$

$$T = \begin{bmatrix} n_x & s_x & a_x & p_x \\ n_y & s_y & a_y & p_y \\ n_z & s_z & a_z & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Representing forward kinematics

- Yaw-Pitch-Roll representation for orientation

$$T_0^n = \begin{bmatrix} C\phi C\theta & C\phi S\theta S\psi - S\phi C\psi & C\phi S\theta C\psi + S\phi S\psi & p_x \\ S\phi C\theta & S\phi S\theta S\psi + C\phi C\psi & S\phi S\theta C\psi - C\phi S\psi & p_y \\ -S\theta & C\theta S\psi & C\theta C\psi & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_0^n = \begin{bmatrix} n_x & s_x & a_x & p_x \\ n_y & s_y & a_y & p_y \\ n_z & s_z & a_z & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

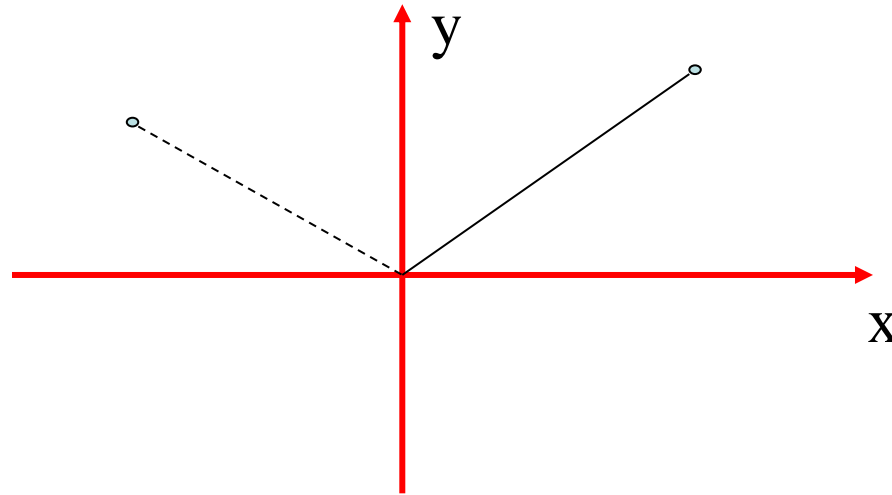
$$\theta = \sin^{-1}(-n_z)$$

$$\psi = \cos^{-1}\left(\frac{a_z}{\cos\theta}\right)$$

$$\phi = \cos^{-1}\left(\frac{n_x}{\cos\theta}\right)$$

Problem? Solution is inconsistent and ill-conditioned!!

# atan2(y,x)



$$\theta = \text{atan2}(y, x) = \begin{cases} 0^\circ \leq \theta \leq 90^\circ & \text{for } +x \text{ and } +y \\ 90^\circ \leq \theta \leq 180^\circ & \text{for } -x \text{ and } +y \\ -180^\circ \leq \theta \leq -90^\circ & \text{for } -x \text{ and } -y \\ -90^\circ \leq \theta \leq 0^\circ & \text{for } +x \text{ and } -y \end{cases}$$



# Yaw-Pitch-Roll Representation

$$T = R_{z,\phi} R_{y,\theta} R_{x,\psi}$$

$$= \begin{bmatrix} C\phi & -S\phi & 0 & 0 \\ S\phi & C\phi & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} C\theta & 0 & S\theta & 0 \\ 0 & 1 & 0 & 0 \\ -S\theta & 0 & C\theta & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & C\psi & -S\psi & 0 \\ 0 & S\psi & C\psi & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
$$= \begin{bmatrix} n_x & s_x & a_x & 0 \\ n_y & s_y & a_y & 0 \\ n_z & s_z & a_z & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Yaw-Pitch-Roll Representation

$$R_{z,\phi}^{-1}T = R_{y,\theta}R_{x,\psi}$$

$$\begin{bmatrix} C\phi & S\phi & 0 & 0 \\ -S\phi & C\phi & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} n_x & s_x & a_x & 0 \\ n_y & s_y & a_y & 0 \\ n_z & s_z & a_z & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad \text{(Equation A)}$$
$$= \begin{bmatrix} C\theta & 0 & S\theta & 0 \\ 0 & 1 & 0 & 0 \\ -S\theta & 0 & C\theta & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & C\psi & -S\psi & 0 \\ 0 & S\psi & C\psi & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

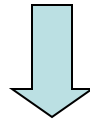
# Yaw-Pitch-Roll Representation

- Compare LHS and RHS of Equation A, we have:

$$-\sin \phi \cdot n_x + \cos \phi \cdot n_y = 0 \quad \Longrightarrow \quad \phi = a \tan 2(n_y, n_x)$$

$$\begin{cases} \cos \phi \cdot n_x + \sin \phi \cdot n_y = \cos \theta \\ n_z = -\sin \theta \end{cases} \quad \Longrightarrow \quad \theta = a \tan 2(-n_z, \cos \phi \cdot n_z + \sin \phi \cdot n_y)$$

$$\begin{cases} -\sin \phi \cdot s_x + \cos \phi \cdot s_y = \cos \psi \\ -\sin \phi \cdot a_x + \cos \phi \cdot a_y = -\sin \psi \end{cases}$$



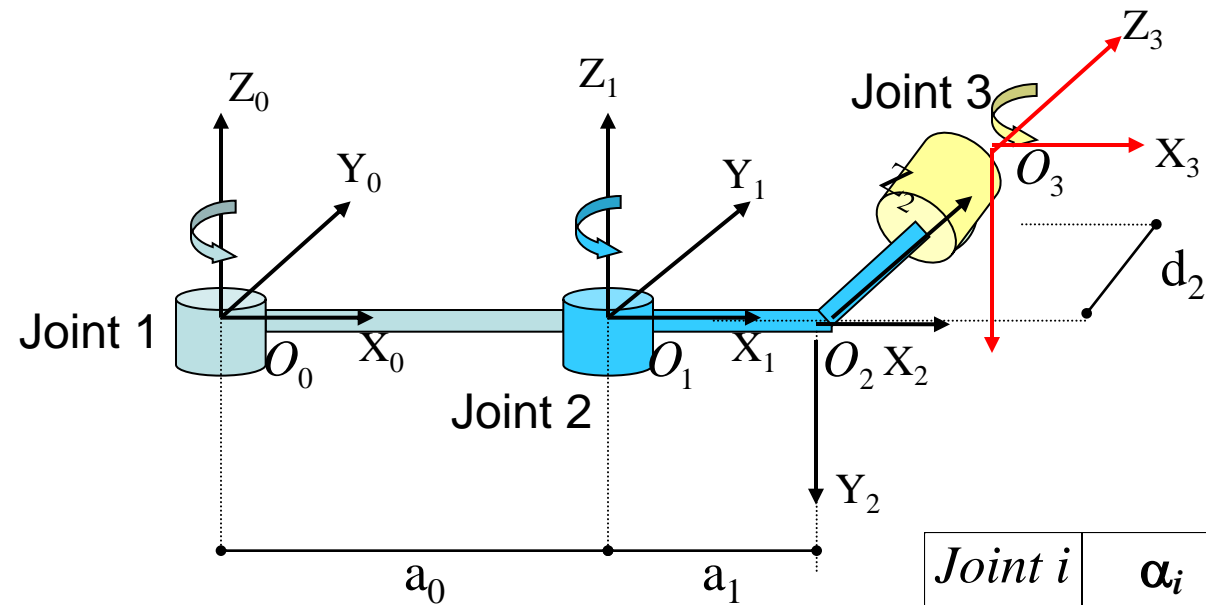
$$\psi = a \tan 2(\sin \phi \cdot a_x - \cos \phi \cdot a_y, -\sin \phi \cdot s_x + \cos \phi \cdot s_y)$$

# Kinematic Model

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- Steps to derive kinematics model:
  - Assign D-H coordinates frames
  - Find link parameters
  - Transformation matrices of adjacent joints
  - Calculate Kinematics Matrix
  - When necessary, Euler angle representation

# Example



<i>Joint i</i>	$\alpha_i$	$a_i$	$d_i$	$\theta_i$
1	0	$a_0$	0	$\theta_0$
2	-90	$a_1$	0	$\theta_1$
3	0	0	$d_2$	$\theta_2$

# Example

Joint $i$	$\alpha_i$	$a_i$	$d_i$	$\theta_i$
1	0	$a_0$	0	$\theta_0$
2	-90	$a_1$	0	$\theta_1$
3	0	0	$d_2$	$\theta_2$

$$T_{i-1}^i = \begin{bmatrix} C\theta_i & -C\alpha_i S\theta_i & S\alpha_i S\theta_i & a_i C\theta_i \\ S\theta_i & C\alpha_i C\theta_i & -S\alpha_i C\theta_i & a_i S\theta_i \\ 0 & S\alpha_i & C\alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

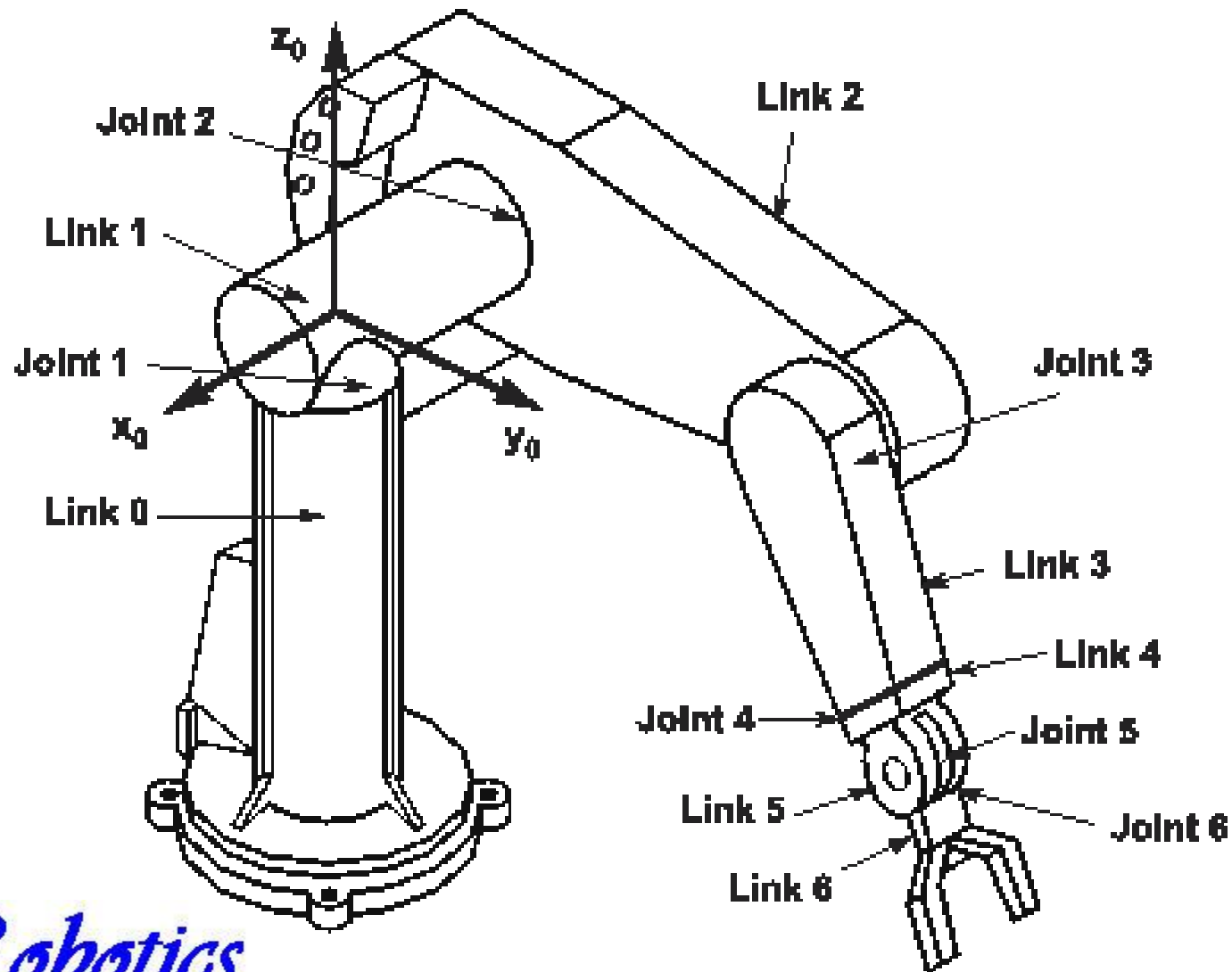
$$T_0^3 = (T_0^1)(T_1^2)(T_2^3)$$

$$T_0^1 = \begin{bmatrix} \cos\theta_0 & -\sin\theta_0 & 0 & a_0 \cos\theta_0 \\ \sin\theta_0 & \cos\theta_0 & 0 & a_0 \sin\theta_0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

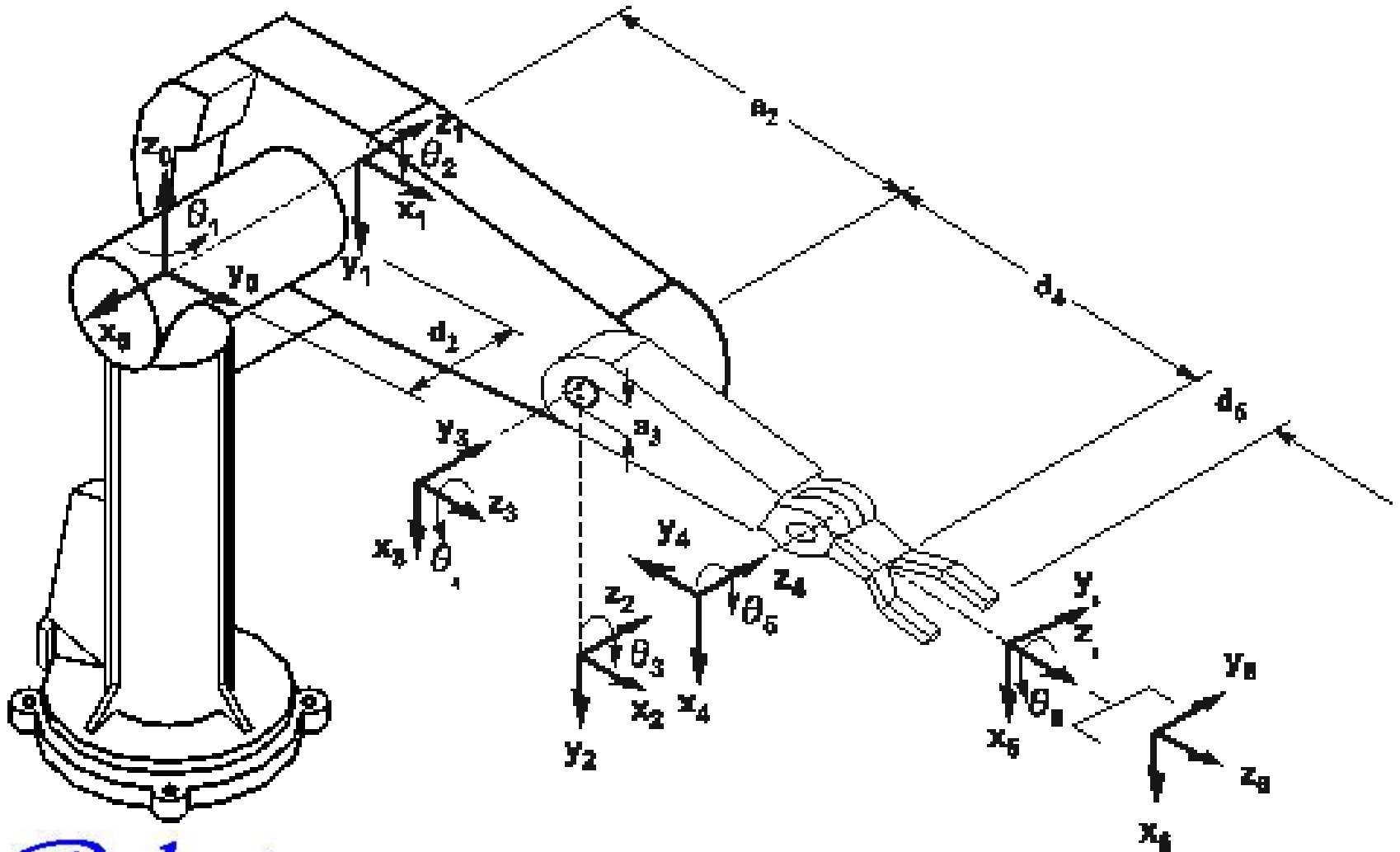
$$T_1^2 = \begin{bmatrix} \cos\theta_1 & 0 & -\sin\theta_1 & a_1 \cos\theta_1 \\ \sin\theta_1 & 0 & \cos\theta_1 & a_1 \sin\theta_1 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$T_2^3 = \begin{bmatrix} \cos\theta_2 & -\sin\theta_2 & 0 & 0 \\ \sin\theta_2 & \cos\theta_2 & 0 & 0 \\ 0 & 0 & 1 & d_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

# Example: Puma 560



# Example: Puma 560



*Robotics*



# Link Coordinate Parameters

PUMA 560 robot arm link coordinate parameters

<i>Joint <math>i</math></i>	$\theta_i$	$\alpha_i$	$a_i(mm)$	$d_i(mm)$
1	$\theta_1$	-90	0	0
2	$\theta_2$	0	431.8	149.09
3	$\theta_3$	90	-20.32	0
4	$\theta_4$	-90	0	433.07
5	$\theta_5$	90	0	0
6	$\theta_6$	0	0	56.25

# Example: Puma 560

$${}^0T_1 = \begin{pmatrix} \cos \theta_1 & 0 & -\sin \theta_1 & 0 \\ \sin \theta_1 & 0 & \cos \theta_1 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^1T_2 = \begin{pmatrix} \cos \theta_2 & -\sin \theta_2 & 0 & a_2 \cos \theta_2 \\ \sin \theta_2 & \cos \theta_2 & 0 & a_2 \sin \theta_2 \\ 0 & 0 & 0 & d_2 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^2T_3 = \begin{pmatrix} \cos \theta_3 & 0 & \sin \theta_3 & a_3 \cos \theta_3 \\ \sin \theta_3 & 0 & -\cos \theta_3 & a_3 \sin \theta_3 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^3T_4 = \begin{pmatrix} \cos \theta_4 & 0 & -\sin \theta_4 & 0 \\ \sin \theta_4 & 0 & \cos \theta_4 & 0 \\ 0 & -1 & 0 & d_4 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^4T_5 = \begin{pmatrix} \cos \theta_5 & 0 & \sin \theta_5 & 0 \\ \sin \theta_5 & 0 & -\cos \theta_5 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^5T_6 = \begin{pmatrix} \cos \theta_6 & -\sin \theta_6 & 0 & 0 \\ \sin \theta_6 & \cos \theta_6 & 0 & 0 \\ 0 & 0 & 1 & d_6 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

# Example: Puma 560

$${}^0T_6 = {}^0T_1 {}^1T_2 {}^2T_3 {}^3T_4 {}^4T_5 {}^5T_6 = \begin{pmatrix} n_x & s_x & a_x & p_x \\ n_y & s_y & a_y & p_y \\ n_z & s_z & a_z & p_z \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$n_x = c_1(c_{23}(c_4c_5c_6 - s_4s_6) - s_{23}s_5c_6) - s_1(s_4c_5c_6 + c_4s_6)$$

$$n_y = s_1(c_{23}(c_4c_5c_6 - s_4s_6) - s_{23}s_5c_6) + c_1(s_4c_5c_6 + c_4s_6)$$

$$n_z = -s_{23}(c_4c_5c_6 - s_4s_6) - c_{23}s_5c_6$$

$$s_x = c_1(-c_{23}(c_4c_5s_6 + s_4c_6) + s_{23}s_5s_6) - s_1(-s_4c_5s_6 + c_4c_6)$$

$$s_y = s_1(-c_{23}(c_4c_5s_6 + s_4c_6) + s_{23}s_5s_6) + c_1(-s_4c_5s_6 + c_4c_6)$$

$$s_z = s_{23}(c_4c_5s_6 + s_4c_6) - c_{23}s_5s_6$$

$$a_x = c_1(c_{23}c_4s_5 + s_{23}c_5) - s_1s_4s_5$$

$$a_y = s_1(c_{23}c_4s_5 + s_{23}c_5) + c_1s_4s_5$$

$$a_z = -s_{23}c_4s_5 + c_{23}c_5$$

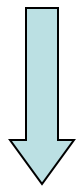
$$p_x = c_1(d_6(c_{23}c_4s_5 + s_{23}c_5) + s_{23}d_4 + a_3c_{23} + a_2c_2) - s_1(d_6s_4s_5 + d_2)$$

$$p_y = s_1(d_6(c_{23}c_4s_5 + s_{23}c_5) + s_{23}d_4 + a_3c_{23} + a_2c_2) + c_1(d_6s_4s_5 + d_2)$$

$$p_z = d_6(c_{23}c_5 - s_{23}c_4s_5) + c_{23}d_4 - a_3s_{23} - a_2s_2$$

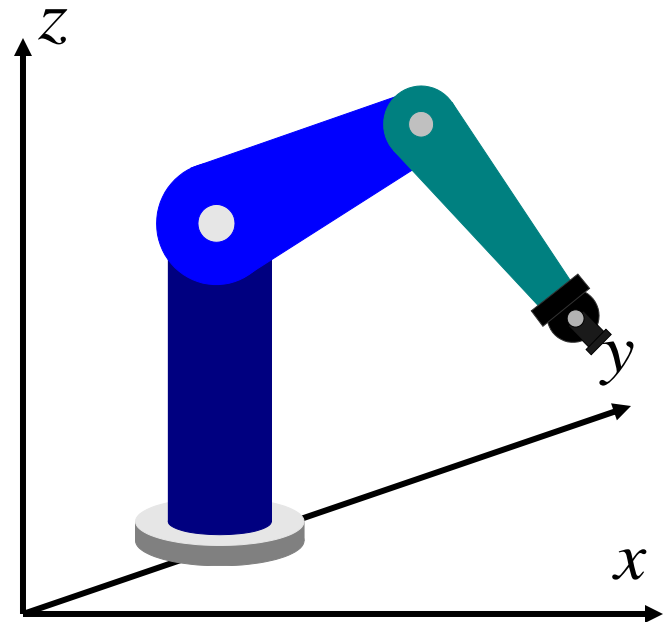
# Inverse Kinematics

- Given a desired position (P) & orientation (R) of the end-effector



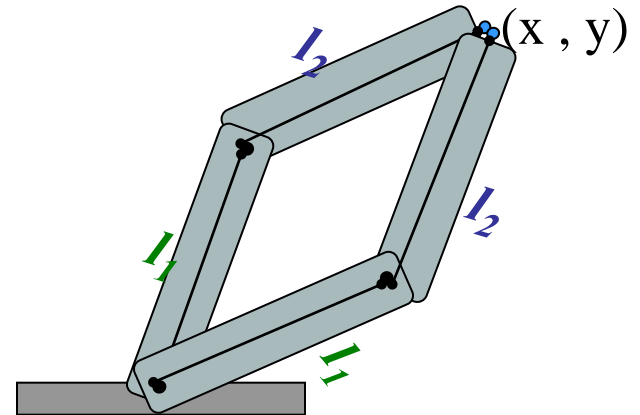
$$q = (q_1, q_2, \dots, q_n)$$

- Find the joint variables which can bring the robot the desired configuration



# Inverse Kinematics

- More difficult
  - Systematic closed-form solution in general is not available
  - Solution not unique
    - Redundant robot
    - Elbow-up/elbow-down configuration
  - Robot dependent



# Inverse Kinematics

- Transformation Matrix

$$T = \begin{bmatrix} n_x & s_x & a_x & p_x \\ n_y & s_y & a_y & p_y \\ n_z & s_z & a_z & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix} = T_0^1 T_1^2 T_2^3 T_3^4 T_4^5 T_5^6 \longrightarrow \begin{bmatrix} \theta_1 \\ \theta_2 \\ \theta_3 \\ \theta_4 \\ \theta_5 \\ \theta_6 \end{bmatrix}$$

Special cases make the closed-form arm solution possible:

1. Three adjacent joint axes intersecting (PUMA, Stanford)
2. Three adjacent joint axes parallel to one another (MINIMOVER)

# Thank you!

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Homework

posted on my web site.

